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A CONTOUR ROUTINE WITH AUTO-INTERPOLATION

M. WIRTH SEISMIC DATA LABORATORY

AUGUST 24. 1971



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Washington, D.C.

Under Project VELA UNIFORM

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Unclassified Security Classification	
	NTROL DATA - R&D
(Security classification of little, body of abeliect and indexi	ing annotation must be entered when the overall report to classified?
I ORIGINATING ACTIVITY (Corporale author)	20. REPORT SECURITY CLASSIFICATION Unclassified
TELEDYNE GEOTECH	26 GROUP
ALEXANDRIA, VIRGINIA	
3 REPORT TITLE	
A CONTOUR ROUTINE WITH	AUTO-INTERPOLATION
4. DESCRIPTIVE NOTES (Type of report and inclusive dates)	
Scientific S. AUTHOR(5) (Lest name, Eral name, Intital)	
Wirth, Mark	
WITCH, MATK	
	Te. TOTAL NO. OF PAGES Th. NO. OF REFS
24 August 1971	29
SE CONTRACT OR GRANT NO.	Se. ORIGINATOR'S REPORT NUMBER(S)
F33657-72-C-0009	0.7.0
B. PROJECT NO. VELA T/2706	272
	Sb. OTHER REPORT NO(S) (Any other numbers that may be seet med this report)
ÅRPA Order No. 1714	thie report)
ARPA Program Code No. 2F-10	•
This document is Approved i	for Public Release; deach trans
milital to for gign Distribu	ution Unlimited be made only
Aith prior approv	12. SPONSORING MILITARY ACTIVITY
II IUPPLEMENTANT NOTES	Advanced Research Projects Agency
C-	Nuclear Monitoring Research Office
	Washington, D. C.
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14 KEY WORDS	
Contour plotting	

A CONTOUR ROUTINE WITH AUTO-INTERPOLATION SEISMIC DATA LABORATORY REPORT NO. 272

VELA T/2706 AFTAC Project No.:

Project Title: Seismic Data Laboratory

ARPA Order No.: 1714

ARPA Program Code No.: 2F-10

Name of Contractor: TELEDYNE GEOTECH

Contract No.: F33657-72-C-0009

Date of Contract: 01 July 1971

Amount of Contract: \$ 1,290,000

Contract Expiration Date: 30 June 1972

Royal A. Hartenberger (703) 836-7647 Project Manager:

P. O. Box 334, Alexandria, Virginia

and each

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ABSTRACT

An efficient contour-plotting routine is discussed which is based on a scanning algorithm of Cottafava and LeMoli and employs bi-linear interpolation. An auto-interpolation scheme is developed which automatically adjusts the number of interpolations in any data square to produce smooth line segments. A program listing and examples are given.

TABLE OF CONTENTS

	Page No.
ABSTRACT	
INTRODUCTION	1
SCANNING ALGORITHM	3
INTERPOLATION	5
AUTO-INTERPOLATION	8
SINGULARITIES AND SADDLE-POINTS	14
RECTANGULAR MESH	15
EXAMPLES	16
REFERENCE	17

LIST OF FIGURES

Figure Title	Figure	No.
Intersection flags	1	
Interpolation conventions	2	
Case I	3	
Case II	4	
Deviation from a chord	5	
Contours in a saddle square	6	
Example 1, real data	7	
Example 2, random numbers	8	

1/

INTRODUCTION

There are many approaches to producing contour maps on a digital computer. Several of these are described by Cottafava and LeMoli (1969). Ideally, a contour routine should be efficient on both computer and plotter, but most seem to possess only one kind of efficiency. For quite a number of reasons, including plotting efficiency, algorithms of the "line-following" type are preferable for use with mechanical plotters. Cottafava and LeMoli present a scanning algorithm of this type which is also very efficient on the computer.

In their program (Cottafava and LeMoli, private communication) they assumed a linear variation between points, but did not do any interpolation in the interior of the data square (defined by four contiguous data points as vertices). Thus a plot produced with their routine consists entirely of straight line segments joined together, the coarseness depending on the spacing of data points. To remedy this, the author developed an autointerpolation scheme employing bi-linear interpolation for use in the interior of the data square. With this scheme, described in the present paper, the number of interpolations used in crossing the data square is automatically adjusted to produce a smooth curve, the number required depending on the curvature of the line segment. This method requires no additional storage and is very fast.

While the interpolation does indeed produce smooth line segments, slope discontinuities sometimes occur on the edges (of the data squares). This is a limitation of the bi-linear interpolation law. An easy and economical solution to this problem is to obtain a finer data mesh by performing a higher-order interpolation before entering the contour routine. This

may also be done when the data are not given as a set of equally-spaced points.

SCANNING ALGORITHM

The scanning algorithm used is that of Cottafava and LeMoli, with several modifications by this author. A more complete discussion than will be given here can be found in the paper cited. For each contour value, the procedure is to scan the entire data array to find which line segments are intersected by the level line and to store the information as flags within the data words themselves. A horizontal and vertical segment are associated with each data point as shown in Figure 1 (the y-axis is given its normal sense here; Cottafava and LeMoli reverse it).

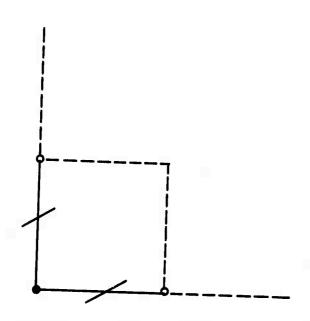


Figure 1. Intersection flags

The flags are stored as bits in the upper part of the integer word, the data being normalized to positive integers by a linear

transformation. (In deference to readers with machines which cannot perform masks, the use of masks in the programs has been limited to an inessential role, where they can easily be replaced by a test and subtract. Where masking statements are available, the flags can be conveniently stored as the least-significant bits of the floating-point mantissa of each data word. This results in a considerable simplification of the program.)

The contours are traced in a second scanning operation, each flag being erased as it is found. This procedure makes it easy to find all the branches of the contour level and is in large part responsible for the efficiency of the program. Each line is traced square by square by a local scan which checks all the edges of the data square in fixed order (counter-clockwise beginning with the right edge) to find the continuation of the line. This procedure runs into trouble only in the case of an interior saddle point (square crossed twice by the same contour), and in this case there is an easy solution based on the interpolation method.

INTERPOLATION

In order to define the behavior of the contour line inside each data square, we must make an assumption about the behavior of the function inside the square. Lacking any special information in the general case, we assume bi-linear variation as the simplest general variation. (Using a higher order interpolation here would also cause serious difficulties with the scanning procedure.) That is, we assume

$$F(x,y) = A + \beta x + \alpha y + \delta x y \tag{1}$$

referred to a local coordinate system with origin at A, as shown in Figure 2.

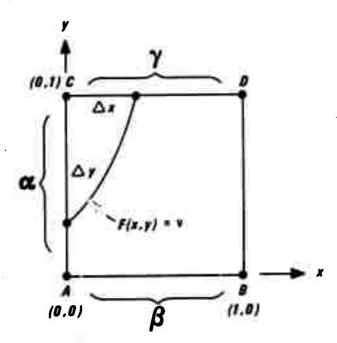


Figure 2. Interpolation conventions

Equation (1) is the Lagrange 2 \times 2 interpolation formula and is also equivalent to a Taylor's series expansion, with the assumption of constant first derivatives on each edge. Making our square of unit dimensions, the derivatives are

$$\alpha \equiv C \stackrel{\cdot}{=} A$$

$$\beta \equiv B - A$$

$$\gamma \equiv D - C$$

$$\delta \equiv \gamma - \beta$$
(2)

With these definitions, it is easy to see that (1) reduces to the correct values at the corners and reduces to ordinary linear interpolation on each edge. Our contour segment is therefore the locus F(x,y) = v, the value of the contour. From (1) we obtain either

$$y = \frac{v - A - \beta x}{\alpha + \delta x} \tag{3}$$

or

$$x = \frac{v - A - \alpha y}{\beta + \delta y} \tag{4}$$

with $0 \le x \le 1$ and $0 \le y \le 1$. These expressions are easily computed. In practice, we choose the number of interpolations, subdivide

 Δx or Δy , and use either (3) or (4), respectively. It is convenient to use (3) for a line terminating on a vertical edge, and (4) for a line terminating on a horizontal edge.

AUTO-INTERPOLATION

We approximate our ideally smooth curve by a series of chords. If we choose the number of chords in each square so that the maximum deviation from the ideal curve is on the order of the basic plotter increment, then we obtain as smooth a curve as we can with no wasted time. We take as our auto-interpolation criterion, the maximum perpendicular distance from the curve to the straight line between the end points. The perpendicular distance from a point to a line is

$$\varepsilon(x) = (y - mx - b) / \sqrt{m^2 + 1}$$
 (5)

from elementary geometry. We consider the case of a segment terminating on the <u>left</u> edge of the square, and for this case there are just two distinct possibilities, as shown in Figures 3 and 4. All other possibilities can be found by reflections and a rotation.

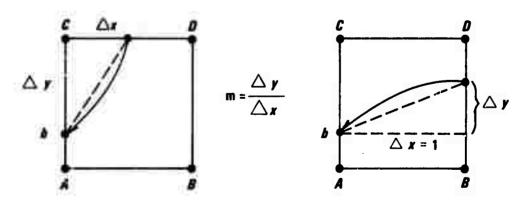


Figure 3. Case I

Figure 4. Case II

For case I the slope is

$$m_1 = \frac{v-C}{C-A} / \frac{v-C}{C-D} = -\gamma/\alpha$$

For case II,

$$m_2 = \frac{v - A - \beta}{\alpha + \delta} - \frac{v - A}{\alpha} = -\frac{\delta(v - A) + \alpha\beta}{\alpha(\alpha + \delta)}$$

For both cases the intercept is $b=(v-A)/\alpha$. The "brute force" calculation of the maximum of (5) is messy, but a transformation simplifies the algebra. Define

$$\eta_{1} \equiv \frac{\delta(v-C)}{\alpha \gamma}$$

$$\eta_{2} \equiv \delta/\alpha$$

$$\eta \equiv \frac{\delta}{\alpha} \Delta x \text{ where } \Delta x = \begin{cases} (v-C)/\gamma, \text{ case } I \\ 1, \text{ case } II \end{cases}$$

Then

$$\frac{\delta(v-A)}{\alpha} + \beta = \delta[1 + \frac{v-C}{\alpha}] + \beta = \gamma[1 + \eta_1]$$

which leads to the relation

$$m_2(1+\eta_2) = m_1(1+\eta_1)$$
 (7)

It can also be shown that

$$y-b = \frac{m_1(1+n_1)}{1+n_2x} x$$

and

$$y' \equiv \frac{dy}{dx} = \frac{m_1(1+n_1)}{(1+n_2x)^2}$$

The location of the maximum of (5) is given by the condition

$$\varepsilon^{\dagger}(\hat{x}) = 0 = y^{\dagger}(\hat{x}) - m$$

(hats will be used to refer to the maximum), i.e.,

$$\frac{m_1(1+n_1)}{(1+n_2\hat{x})^2} = m \tag{8}$$

Thus

$$\hat{y}$$
-b = m(1+ $\eta_2\hat{x}$) \hat{x}

and

$$\sqrt{\hat{m}^2 + 1} \hat{\epsilon} = \hat{y} - b - m\hat{x} = m\eta_2 \hat{x}^2$$

or

$$\hat{\varepsilon} = \frac{m}{\sqrt{m^2 + 1}} \eta_2 \hat{x}^2 \tag{9}$$

where \hat{x} is found from (8). For case I, m = m₁, and

$$\hat{x}_1 = \frac{1}{\eta_2} \left[\sqrt{1 + \eta_1} - 1 \right]$$

For case II, $m = m_2$, and using (7) in (8) gives

$$\hat{x}_2 = \frac{1}{\eta_2} [\sqrt{1 + \eta_2} - 1]$$

which has the same form. Putting these results in (9) gives

$$\hat{\varepsilon} = \frac{m}{\sqrt{m^2 + 1}} \frac{1}{\eta_2} \left[\sqrt{1 + \eta} - 1 \right]^2$$

for both cases. This is conveniently written in the form

$$\hat{\varepsilon} = \frac{\Delta x \Delta y}{\sqrt{\Delta x^2 + \Delta y^2}} \left\{ \frac{1}{\eta} \left(\sqrt{1 + \eta} - 1 \right)^2 \right\}$$
 (10)

Since (10) is symmetric in x and y, it can be easily seen to apply to the case of a segment terminating on the bottom edge of the square also, provided that we define $\eta \equiv \delta \Delta y/\beta$ in this case. Thus all possible cases are contained in (10). A bound can be placed on $\hat{\epsilon}$ by considering $\eta \rightarrow \infty$ and $\Delta x \rightarrow \Delta y \rightarrow 1$, namely $\hat{\epsilon} < 1/\sqrt{2}$, which agrees with geometrical intuition.

Knowing how to calculate the maximum deviation of the curve from the straight line between endpoints, we use this to estimate the number of segments needed to approximate the curve to any desired accuracy. To do this, we consider the case of a circular arc, Figure 5.

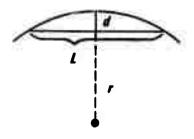


Figure 5. Deviation from a chord

It is easily shown that $d\approx L^2/8r$, provided L/r<<1, the important point being the proportionality $d \propto L^2$. Since L \propto 1/N, approximately, where N is the number of segments needed in that square, we take

 $N = 1 + \sqrt{\epsilon/d}$

where d equals the allowable deviation. For plotters with a 2.5 mil increment, d=.001" is satisfactory. This auto-interpolation scheme appears to work quite well.

SINGULARITIES AND SADDLE-POINTS

Evidently something peculiar happens with (10) if $\eta+1<0$. This can be seen to be connected with a singularity in y or x, equation (3) or (4). The existence of a singularity in y(x)within the interval $0 \le x \le 1$ is implied by the condition that (D-B) and $\boldsymbol{\alpha}$ have opposite signs, and the existence of a singularity in x(y) within the interval $0 \le y \le 1$ is implied by the condition that γ and β have opposite signs. If both singularities exist, then the square has an interior saddle point located at the intersection. An example is shown in Figure 6. A very convenient criterion for making connections in a saddle square is that contours should never cross a singularity. The condition $\eta+1<0$ can be easily shown to imply a wrong connnection in a saddle square. By far the easiest solution to this problem is just to check for a wrong connection and to resume scanning the square if it exists. At most three tries will be necessary to make the correct connection, and since saddle-points should be relatively rare, this is a small price to pay for such a simple procedure that guarantees correct connections.

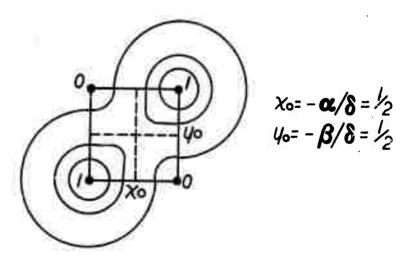


Figure 6. Contours in a saddle square

RECTANGULAR MESH

Should it be desired to plot data cells as rectangles instead of squares, this is easily done by stretching one axis in the calls to PLOT. Defining r as the ratio of x to y scale factors, i.e. the rectangle has length r in the x-direction and l in the y-direction, elementary trigonometry gives for the modified deviation

$$\tilde{\epsilon} = \epsilon \sqrt{\frac{1+r^2m^2}{1+m^2}} = \epsilon \sqrt{\frac{\Delta x^2+r^2\Delta y^2}{\Delta x^2+\Delta y^2}}$$

EXAMPLES

Two simple examples of plots produced by the routine are shown in Figures 7 and 8. Figure 7 was produced from real, deterministic, data, and Figure 8 from random numbers. Data points are marked by ticks along the borders of the plots. Each plot is based on only 24 data points, and the large number of slope discontinuities indicates the need for a more refined data mesh.

REFERENCE

Cottafava, G. and LeMoli, G., 1969, Automatic contour map: Comm. ACM 12(July), p. 386-391.

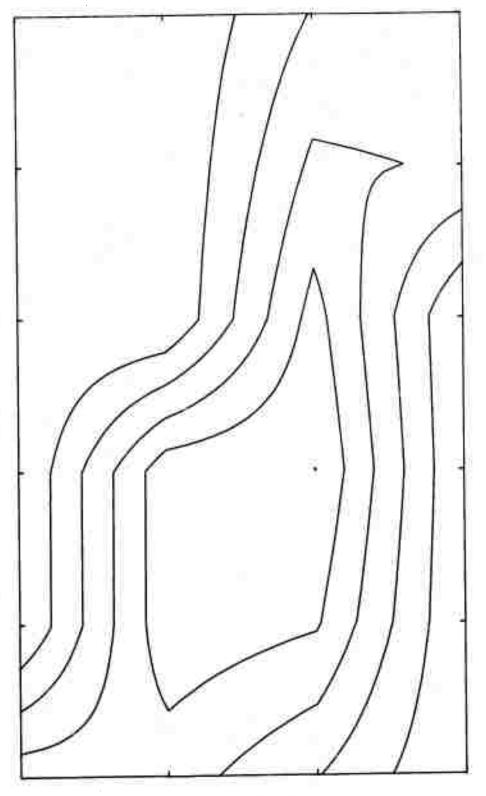


Figure 7. Example 1, real data

-18-

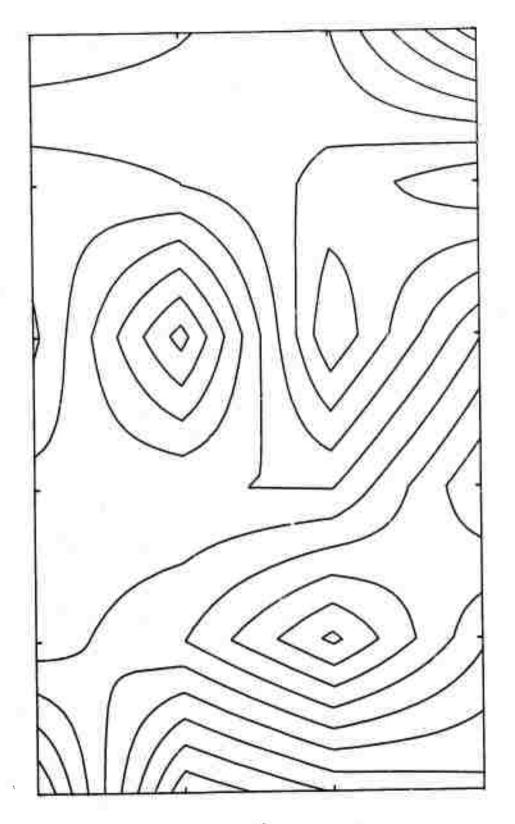


Figure 8. Example 2, random numbers

-19-

APPENDIX

PROGRAM LISTING

Written in FORTRAN-63, a programming language of the CDC 1604 computer. Integer words assumed at least 33 bits long.

```
SUBROLTINE CONTORT M.N.F. K.C. ND.NDZ.IV.IA, HEIGHT, DEV )
      BIMENSION C(K), F(ND,M), LV(NU2,M), IA(M)
      BATA (IHOR = 100000000000) (IVER = 200000000000)
     PLOT CONTOURS F(1,J) = F(T,X) = C. [=1.N. 3 J=1.M
      SV S IA ARE AUXILIARY ARRAYS. HAY EUUIVALENCE (F.IV.
C
      MUST HAVE ND2 2 N+2
      ADEV+ IS AUTO-INTERPOLATION PANAMETER = APPROX. ALLOWABLE DEV.
      CINCHES). SUGGEST DEV = :001
ALGORITHM BY COTTAFAVA & LEHOLI, POLITECNICO DI MILANO.
      TRANSCRIRED & HEVISE'S BY MARK MINTH, JANUARY 1971.
BRITERPOLATION ALGURITHM BY MARK WINTH
C
      NORMALIZE DATA
      MMAX . F
                                FMIN = U.
      80 5 J = 1.H
      10 5 1 = 1.N
    1 RMAX = F([.J)
                                60 10
      BFC F(I,J).LT.PHIN ) 3.5
    3 \text{ PHIN} = F(I,J)
    5 GONTINUE
                                                      H = - MIN+A +.5
       4 = 16+8/(FMAX-FMIN)
       80 8 J = 1.M
       80 7 1 = 1.N
    7 3V(1+1,JR) = A*F(1,JR-1) + 8
       1V(1,JR) = [V(NP2,JR) = n
    B AR B JR - ;
BALL ERASET NP2. 14 )
       BALL ERASE( NP2, IV(1, M+2) )
       MAC = HEIGHT/(N-1)
                                                      DEVS = DEV / FAC
       BALL FACTOR ( FAC )
      LOOP OVER CONTOUR LEVELS
C
       10 500 L = 1,K
       NO . IVOL . A.L(L) + B
       ARELININARY SCAN. SET FLAGS
C
       10 20 J = [V.2.3) - IVOL
   IF( IA(J) ) 20 10 $ 10 10 GONTINUE
                                IA(5)AI = IA(5)AI +
       60 100 I = 2,N1
       11 . 1 . 1
       80 100 J = 2,M1
       3F( 1.EQ.N1 ) $0.60
   30 1C = IV([1,J) - IVOL
       BF( 10 ) 40,35
                                T + (PILLIAT = (PILLA) + T
   35 1C = 1
   40 BF( XSIGNF(1, IA(J))+IC ) 50.50.60
   50 \text{ IV(I,J)} = \text{IV(I+J)} + \text{IVER}
   60 JF( J.EQ.M1 ) 100.70
   70 IF ( XSIGNF(1, [A(J))*[A(J+1) ) *0.80.100
    80 IV(I, \omega) = IV(I, \omega) + IHOR
  100 M(J) = 10
```

```
RICK UP RHANCHES UF CONTOUR LEVEL
C
        00 200 J = 2.M

00TTOM EDGE

IIV = IV(2.J).AND.NOT.IVEH
C
  170 ONLL BHANCH( 2.J.1.1. ND2, 14, 40, DEVS )
        POP EUGE
 130 IF( IV(N1.J) GE. IHOR ) 140.200
  140 GALL BHANCH( N1.J.1.2, ND2.14.40.DEV5 )
  200 CONTINUE
        RIGHT EDGE
  #0 300 1 = 2.0

IF( IV(I,M1).GE.IVER ) 250,300

250 GALL BHANCH( I.M1,2,3, ND2,IV,VO,DEVS )
  300 CONTINUE
       WEFT EUGE & INTERIOR
       00 500 J = 2.M
       KK = 2 / J
 #0 500 I = 2.N

# (IV(I,J).LT=IVER ) 500.350

# (IV(I,J).LT=IVER ) 500.350

# (IVI).RKK, ND2.IV.VO.DEVS )
 500 CONTINUE
       GALL FACTUR( 1. )
       METURN
       END
```

```
SUBROUTINE APANCH( THEM, JHEM, LISP, K. NU. IV, VU. DEVS )
    SIMENSION IV(NO.10
    RULLOW ONE BRANCH OF CONTOUR LEVEL
                                                  JY = J = JREM
    IPEN = 3
                                            5
                   3
                        IP = I = IREM
                                                  II . U
                        YP = 1 - 2
                                            5
    #P = u - 2
                   3
                        ASSIGN 1 TO JAIL
                                            5
                                                  GU TU 200
    NISP = LISP
  1 IPFN = 2
    QU TO (5,4,3), K
                                     GU 10 5
  3 JS = 0 = J = 1
4 IS = I = I = 1
  5 IF( IV(I,J+1).GE.IVER ) 10-15
10 d = J+1 % MISP = 2 3
15 IBV = IV(I+1,J).AND..NOT.IVER
IF( IbV.GE.THUR ) 20,25
                                     ASSIGN 5 TO JAIL
                                                               GO TO
                                                         S
                                                                      200
                                                               GO TO
                                     ASSIGN 5 10 JAIL
             $
                   MISP = 1
                                                                      200
   1 = I+1
 25 1F( IV(I,J).GE.IVER ) 30.37
                        ASSIGN & TU JAIL
                                                  GU TU
                                                         20 u
 30 NISP = 2
                3
 35 IF( IV(I,J).Gt.IHOR ) 40.90
 40 NISP . 1
                       ASSIGN 4 TU JAIL
                                            S
                                                  GU TO
                                                         200
 90 IF( K ) 100 - 190
   RETURN
100
    REMOVE FLAGS, INTERPOLATE, AND PLOT POINT
                                                  IA(I'') = IA(I'') DIAEH
                   3
                        J = JREM
    B = IHEM
190
    NISP = 2
                        ASSIGN 100 TO JAIL
                        Yn = 1 - 2
200 10 = J - 2
                   3
                   3
                        10 . IP
    40 = JP
    $F( J.EQ.JP ) 210,220
210 JO . JP +
    1F( 1.EQ. IP ) 230.24
220
   10 = IP + 1
230
   HVI.TON..UNA.(L.I)VI = AI = A
240
    HVI .TON . . GNA . (DL . I) VI . B
      = IC = IV(IU)).AND..NOT.IVH
    HVI. ON. . DNA. (DC. DI) VI = B
                                                  DEL . D-C - BET
    ALF = C - A 3
                        BET = B - A
    40 TO (250,26,), MISP
250 IF = (VO-A)/BET + XO
                                     DX = XF - XP
                                                               VF = YO
                                3
                                     DY = Y = SIGN+(YP-YO)
                                3
    $1GN = 10 - 1
                                     GU 10 270
    BTA = DY+DEL / BET
                                                               XF = XO
260 FF = (VO-A)/ALF + YO
                                5
                                     DX = A = SIGN+(XP+XO)
    $1GN - JO - J
    BTA = DX+DEL / ALF
270 IF( E1A ) 28n+40n
280 STAP * ETA + 1.
SADDLE-POINT TEST
    1F( ETAP ) 290,295,300
                                                  11 = 11 + 1
290 1 = 15
                                            5
                        J = JS
    00 TO (15,25,35), IT
295 EPS = 1. 5 GO TO 310
300 EPS = DX+DY+(SURTE(ETAP)-1:)**2 / (E!A*SURTE(DX+DX+DY+DY))
810 BI . 1.5 + SORTF (ABSF (EPS)/DEVS)
                                    II = 6
    MNI = NI +.9999
    $0 TO (320,350), MISP
```

```
320 BY = Y / FN1
F = VG-A - ALF#Y
G = 8ET + DEL#Y
                                          UF = -ALFAUY
                                          DG = MEL+MY
X = F/G
     GALL PLOT ( X0+X, Y0+SIGN+Y, IPEN )
QO TO 330

350 DX = X / FNI

R = VC-A - RFT+X

Q = ALF + DFL+X
                                          D+ = -8E1+0X
                                          DG = NEL+UX
860 X = X - 1)X
IF( X ) 400,400,370

870 M = F - DF B G = G - DG

GALL PLOT( X0+SIGN+X,Y0+Y, IPEN )
                                                         Y = 5/G
5
                                                   XP = XF
     END
```